

## **(Very) basic elements on parameterization of oceanic and atmospheric turbulence**

*"I am an old man now, and when I die and go to heaven there are two matters on which I hope for enlightenment. One is relativity/quantum mechanics/quantum electrodynamics, and the other is turbulent motion of fluids. About the former I am rather optimistic"*  
(Werner Heisenberg, 1932 Nobel Prize winner)

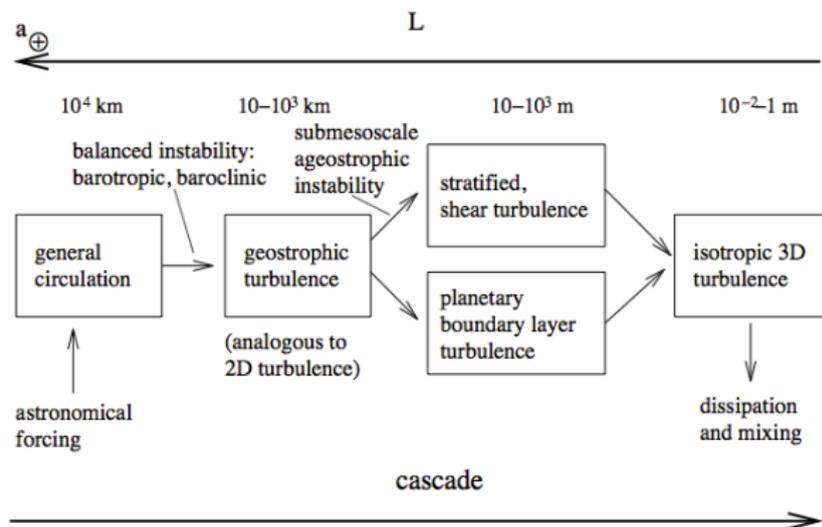
## Context

- **Turbulence:** motions on wide range of scales from a few centimeters to thousand of kilometers that continuously interact
- to develop theories and numerical models of the large-scale circulation, we need to account for these interactions,
- i.e. understand how energy is transferred from the thousand of kilometers scales, to the centimeters scales, where energy is dissipated as heat.

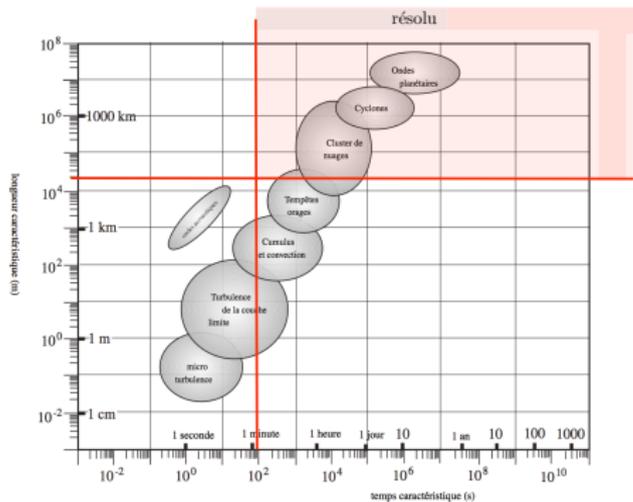
In the case of the oceanic turbulence

1. **From the large-scale currents to the mesoscale eddies.** The large-scale oceanic currents are unstable which generate eddies with scales of 10 to 100 kilometers (the mesoscales).
2. **The mesoscale eddies then interact and generate submesoscale turbulent filaments** on scales from 10 kilometers to 100 meters.
3. Only at scales below approximately 10 meters, **the turbulence becomes three-dimensional** and it is described as stratified microscale turbulence

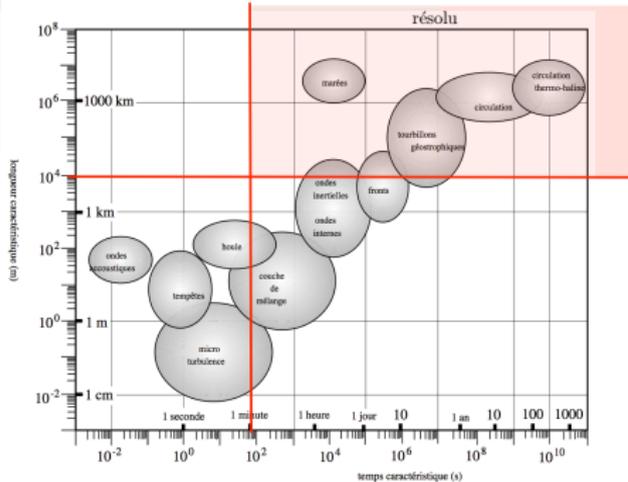
## Context: different turbulent regime



# Context: characteristic scales of physical processes



Atmosphere



Ocean

## General properties

- **From a mathematical perspective**, turbulent behaviors arise because the governing equations of fluid dynamics are a nonlinear partial differential equation (PDE) system
- **From a physical perspective**, the advection causes the generic behavior of the entanglement of neighboring material parcels; this causes chaotic evolution, transport, and mixing.

# 1

## Reynold's decomposition

## Principle

- Governing equations are deterministic, not random

$$\frac{D\mathbf{u}}{Dt} = -\frac{1}{\rho_0} \nabla p + \nu \Delta \mathbf{u} + \widehat{z}b - f\widehat{z} \times \mathbf{u}$$

$$\nabla \cdot \mathbf{u} = 0$$

$$\frac{Db}{Dt} = \kappa \Delta b, \quad b = g(1 - \rho/\rho_0)$$

- However, turbulent motions are generally described using statistical methods considering  $\mathbf{u}$  and  $b$  as random variables
- Reynold's decomposition for  $X = u, v, w, b$ :

$$X = \underbrace{\langle X \rangle}_{\text{mean}} + \underbrace{X'}_{\text{fluctuations}}, \quad \langle X' \rangle = 0$$

## Which filter $\langle \cdot \rangle$ is adequate

- Ensemble average

$$\langle u \rangle_E = \int q(\mathbf{x}, t, \omega) d\omega$$

- Low-pass filter

$$\langle u \rangle_F = \sum_{|\mathbf{k}| \leq k_e} F(q) e^{i\mathbf{k} \cdot \mathbf{x}}$$

- Space averaging

$$\langle u \rangle_B = \frac{1}{|B|} \int_{B(x,r)} u(y, z, t) dy$$

- Time averaging

$$\bar{u} = \frac{1}{T} \int_{t-T}^t u(\mathbf{x}, \tau) d\tau$$

- Space-Time averaging

$$\langle \bar{u} \rangle_B = \frac{1}{T} \int_{t-T}^t \langle u \rangle_B d\tau$$

## Filter properties

	$\langle \cdot \rangle_E$	$\langle \cdot \rangle_F$	$\langle \cdot \rangle_B$	$\bar{\cdot}$	$\langle \bar{\cdot} \rangle_B$
Linearity ( $\langle u + v \rangle = \langle u \rangle + \langle v \rangle$ )	X	X	X	X	X
Derivatives and averages commute	X	X	X	X	X
Double averages ( $\langle \langle u \rangle \rangle = \langle u \rangle$ )	X	X			
Product average ( $\langle v \langle u \rangle \rangle = \langle v \rangle \langle u \rangle$ )	X				

**Only the ensemble averaging satisfies all properties**

**Link with observations and experiments:** turbulence is assumed ergodic

$\Rightarrow$  *The ergodic theorem of probability theory (Neveu[1967]) says that, under certain conditions, statistical means can be replaced by time averages or spatial averages in the case of multidimensional processes.*

## Reynolds averaged equations

$$\partial_t \langle \mathbf{u} \rangle + \langle \mathbf{u} \rangle \cdot \nabla \langle \mathbf{u} \rangle = -\frac{1}{\rho_0} \nabla \langle p \rangle + \nu \Delta \langle \mathbf{u} \rangle + \widehat{\mathbf{z}} \langle b \rangle - f \widehat{\mathbf{z}} \times \langle \mathbf{u} \rangle - \nabla \cdot \langle \mathbf{u}' \mathbf{u}' \rangle$$

$$\nabla \cdot \langle \mathbf{u} \rangle = 0$$

$$\partial_t \langle b \rangle + \langle \mathbf{u} \rangle \cdot \nabla \langle b \rangle = \kappa \Delta \langle b \rangle - \nabla \cdot \langle \mathbf{u}' b' \rangle$$

- eddy momentum flux (a.k.a. Reynolds stress)

$$\mathbf{R} = \begin{pmatrix} \langle u' u' \rangle & \langle u' v' \rangle & \langle u' w' \rangle \\ \langle v' u' \rangle & \langle v' v' \rangle & \langle v' w' \rangle \\ \langle w' u' \rangle & \langle w' v' \rangle & \langle w' w' \rangle \end{pmatrix}$$

- eddy tracer flux  $\mathbf{R}_b = (\langle u' b' \rangle, \langle v' b' \rangle, \langle w' b' \rangle)^T$

⇒ how to close this system ?

## The turbulence closure problem

- **Second-moment closure models**

e.g. under the assumption  $\partial_x \cdot = \partial_y \cdot = 0$

$$\partial_t \langle w' b' \rangle = - \langle w' w' \rangle \partial_z \langle b \rangle - \frac{1}{\rho_0} \langle b' \partial_z p' \rangle - \partial_z \langle w' w' b' \rangle + \dots$$

Second-moments are always function of higher order moments

- **Eddy viscosity/diffusivity models (a.k.a. 1<sup>st</sup>-moment models, K-theory)**

$$\mathbf{R} = \mathbf{R}(\nabla \langle \mathbf{u} \rangle), \quad \mathbf{R}_b = \mathbf{R}_b(\nabla \langle b \rangle)$$

$$\text{Boussinesq assumption : } - \langle \mathbf{u}' \phi' \rangle = K_\phi \nabla \langle \phi \rangle$$

- analogy with molecular viscosity
- Down-gradient fluxes
- Turbulence acts as “mixing”

**How to determine  $K_\phi$  ?**

## Turbulent kinetic energy

Turbulent kinetic energy (TKE) is a measure of the intensity of turbulence defined as

$$\langle e \rangle = \frac{1}{2} (\langle u' u' \rangle + \langle v' v' \rangle + \langle w' w' \rangle)$$

Prognostic equation :

$$\begin{aligned} \partial_t \langle e \rangle + \nabla \cdot (\langle \mathbf{u} \rangle \langle e \rangle + \langle \mathbf{u}' e \rangle + \frac{1}{\rho_0} \langle \mathbf{u}' p' \rangle - \nu \nabla \langle e \rangle) \\ = \underbrace{- \langle u' \mathbf{u}' \rangle \cdot \nabla \langle u \rangle - \langle v' \mathbf{u}' \rangle \cdot \nabla \langle v \rangle - \langle w' \mathbf{u}' \rangle \cdot \nabla \langle w \rangle}_{\text{Shear production}} + \underbrace{\langle w' b' \rangle}_{\text{buoyancy}} - \underbrace{\frac{\nu}{2} \|\nabla \mathbf{u}'\|^2}_{\text{dissipation}} \end{aligned}$$

Closure assumptions :

- $-(\langle \mathbf{u} \rangle \langle e \rangle + \langle \mathbf{u}' e \rangle + \frac{1}{\rho_0} \langle \mathbf{u}' p' \rangle - \nu \nabla \langle e \rangle) = K_e \nabla \langle e \rangle$
- $-\langle u' \mathbf{u}' \rangle = K_u \nabla \langle u \rangle$
- $-\langle w' b' \rangle = K_b \partial_z \langle b \rangle$
- $\varepsilon$ : ultimate dissipation of KE of all motions
  - Kolmogorov (1941) :  $\varepsilon = \langle e \rangle^{3/2} / \Lambda_\varepsilon$
  - Evolution equation for  $\varepsilon$  ( $k$ - $\varepsilon$  closure scheme)

## 1-equation TKE closure

- In ocean/atmosphere models  
→ one-point closures assuming horizontal homogeneity

$$\partial_t \langle e \rangle = \partial_z (K_e \partial_z \langle e \rangle) + K_m \{ (\partial_z \langle u \rangle)^2 + (\partial_z \langle v \rangle)^2 \} - K_b \partial_z b - \langle e \rangle^{3/2} / \Lambda_\varepsilon$$

- It is expected that  $K_\phi$  is related to  $\langle e \rangle$

$$K_m = \Lambda_m \sqrt{\langle e \rangle}, \quad K_b = \Lambda_b \sqrt{\langle e \rangle}, \quad K_e = \Lambda_e \sqrt{\langle e \rangle}$$

where  $\Lambda_\phi$  are turbulent length scales usually derived from a “master length scale”

$$(\Lambda_\varepsilon, \Lambda_m, \Lambda_b, \Lambda_e) = \left( \frac{1}{c_\varepsilon}, C_m, S_b(\partial_z \langle b \rangle), Sc_e \right) \Lambda$$

The master length scale is diagnosed one way or another

Talk by O. Audouin (AMA): parameter control for  $C_m$ ,  $\frac{1}{c_\varepsilon}$ ,  $S_b$ ,  $Sc_e$  and  $\Lambda_{\min}$

## 2-equations turbulence models

- Algebraization of 2-equations closures : Generic Length Scale models

$$\partial_t \langle e \rangle = \partial_z (K_e \partial_z \langle e \rangle) + K_m \{(\partial_z \langle u \rangle)^2 + (\partial_z \langle v \rangle)^2\} - K_b \partial_z b - \varepsilon$$

$$\partial_t \psi = \partial_z (K_\psi \partial_z \psi) + \frac{\psi}{\langle e \rangle} (c_{\psi 1} K_m \{(\partial_z \langle u \rangle)^2 + (\partial_z \langle v \rangle)^2\} - c_{\psi 3} K_b \partial_z b - c_{\psi 2} \varepsilon)$$

$c_{\psi 1}$ ,  $c_{\psi 2}$ ,  $c_{\psi 3}$ , and  $S_{c_\psi}$  determined empirically

- “Generic” aspect: the quantity  $\psi$  is related to the dissipation rate as

$$\varepsilon = (c_0)^{3+p/n} \langle e \rangle^{3/2+m/n} \psi^{-1/n}, \quad \psi = (c_0)^p \langle e \rangle^m \Lambda^n, \quad \Lambda = (c_0)^3 \langle e \rangle^{3/2} \varepsilon^{-1}$$

Depending on the parameter values for the triplet  $(m, n, p)$  the GLS scheme will either correspond to a  $k - \varepsilon$ , a  $k - \omega$ , a  $k - kl$  or the so-called generic turbulence scheme.

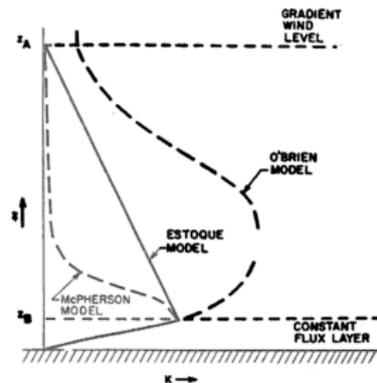
## 0-equation models

- O'Brien (1970, JAS) : for time scales involved in climate models, an equilibrium profile for the vertical structure of the eddy viscosity  $K_m$  is

$$K(z) = P_3(z, z_A, z_B, K(z_A), K(z_B), K'(z_A), K'(z_B))$$

knowing that in the constant flux layer

$$K(z_B) = \kappa u_* z / \phi(z), \quad \phi(z) : \text{stability function}$$



- From TKE equation: intensity of turbulence largely determined by

$$Ri = \frac{\partial_z \langle b \rangle}{(\partial_z \langle u \rangle)^2 + (\partial_z \langle v \rangle)^2}$$

From theoretical and experimental studies :

- Convective instability for  $Ri < 0$
- Non-turbulent flow becomes turbulent when  $Ri \lesssim Ri_{Cr}$
- Turbulent flow becomes non-turbulent when  $Ri \gtrsim 1$

## 0-equation models

Integral view over the boundary layer  $[z_{\text{sfc}}, h_{\text{bl}}] : \text{Ri}_B(h_{\text{bl}}) = \text{Ri}_{\text{cr}}$  with

$$\text{Ri}_B(z) = \frac{(z - z_{\text{sfc}})(\langle b \rangle(z) - \langle b \rangle(z_{\text{sfc}}))}{\|\mathbf{u}(z) - \mathbf{u}(z_{\text{sfc}})\|^2}$$

→ K-profile boundary layer model (Troen & Mahrt (1986); Large et al. (1994))

1. Extent of PBL  $h_{\text{bl}}$  is determined from  $\text{Ri}_B(h_{\text{bl}}) = \text{Ri}_{\text{cr}}$
2. Apply the O'Brien (1970) equilibrium shape function

$$K_{m,b}(z) = w_{m,b} h_{\text{bl}} G(z/h_{\text{bl}})$$

where  $w_{m,s} = \kappa u_* / \phi_{m,s}(z)$  ( $\phi_{m,s}(z)$  are stability functions).

## Turbulent closures in realistic ocean/atmosphere models

	Ocean	Atmosphere
0-equation	Croco, MOM6, MPAS-O	IFS, AR5, LMDZ5
1-equation TKE	NEMO	LMDZ, Arpege, Arome, MesoNH
2-equations	Croco, NEMO, ROMS	MAR ( $k$ - $\epsilon$ )

## Simulation types and turbulent closures

- **DNS (Direct Numerical Simulation)** : all scales are explicitly resolved, no turbulent closures
- **LES (Large Eddy Simulation)** :  $\Delta x \approx 10\text{m}$ , no approximations in model equations + relax one-point closure assumption
- **MILES (Monotonic Implicit Large Eddy Simulation)** :  $\Delta x \approx 10\text{m}$ , no approximations in model equations, no turbulent closures, “Nonlinearly stable” numerical schemes
- **CRM (Cloud Resolving Models)** :  $\Delta x \approx 1 - 2\text{km}$ , no approximations in model equations + 1D or 3D closure

## Parameter estimation

How to provide the reference for parameter estimation

- LES simulations (e.g. HighTunes)
- Observations (assuming ergodicity)
- Laboratory experiments + supporting theory  
(e.g. Kato & Philips, Willis & Deardorff, logarithmic layers, etc.)